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Correlation and prediction of thermodynamic properties of dilute solutes in water up to high T and P. I. Simple fluids He, Ne, Ar, Kr, Xe, Rn, H₂, N₂, O₂, CO, CH₄



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1. Introduction

Thermodynamic properties of components of aqueous solutions at high temperatures and pressures are necessary for both technological applications and for geochemical modeling of water-gasrock interactions. The Helgeson-Kirkham-Flowers (HKF) model is often used to calculate the Gibbs energies and other thermodynamic functions at infinite dilution in water of ions [1,2] and neutral solutes [3] at high T and P. The T-P range of applicability for this model was recently [4] extended to ~1500 K and 6 GPa. Application of the model to neutral (noncharged) species had a limited theoretical basis and was later shown unable to quantitatively reproduce available data at near-critical and supercritical temperatures [5–10]. Equations of state (EoS), with parameter mixing rules in the geochemical literature are more successful at predicting thermodynamic properties, including infinite-dilution fugacity coefficients, ϕ_2^{∞} , (related to Gibbs energies) of dissolved aqueous gases up to very high T and P. These include models from molecular simulation-based PVTx properties of binary water-gas systems

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ABSTRACT

Fugacity coefficients of dilute aqueous solutions of six noble gases and five simple fluids have been correlated from ambient conditions (298 K, 0.1 MPa) to high temperatures (up to 2000 K) and water densities as high as 1500 kg m⁻³. A correlation is developed for the function, $A_{12}^{\infty} = V_2^{\infty}/\kappa_T RT$, that includes known constraints: second virial coefficients at low-water densities, rigid-body behavior at highwater densities, near-critical principles, and corresponding-states relations. Reasonable agreement with an extensive, evaluated database of volumetric and solubility measurements has been achieved over the entire range of conditions, though comparisons of calculated with recommended Henry's constants suggest reconsiderations of recommendations for He and CO at temperatures above 550 K.

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[11,12], from perturbation theory [13], and others. Several literature EoS have been coded by R.J. Bakker [14] and may be freely downloaded from: http://fluids.unileoben.ac.at/Computer.html. Our analyses [9,10,15] show general agreement of results of these EoS up to water densities of $\sim 1000 \text{ kg m}^{-3}$, although the differences significantly increase - up to ~3 log10 units - at pressures in excess of 5-6 GPa. Since these EoS are intended for the use at supercritical temperatures, their applications at subcritical temperatures, reported mostly as Henry's constants, $k_{\rm H}$, are problematic. In addition, such "classical" EoS cannot accurately describe properties in the near-critical region where long-range density and composition fluctuations arise [16]. These issues suggest developing property models from alternative concepts.

One approach is to model derivative partial molar properties, particularly the partial molar volume, V_2^{∞} , and use thermodynamic manipulations to establish expressions for partial molar heat capacities, $C_{n,2}^{\infty}$, and $k_{\rm H}$ [8,17,18]. The basis for this was suggested in Ref. [7]. These models closely reproduce precise V_2^{∞} results over the whole temperature range of measurements, from 298.15 up to 720 K, at pressures up to 40 MPa. It has been recently shown that early formulations are less reliable for extrapolation to higher temperatures and densities/pressures [9,15]. A method consistent with known theoretical constraints (at low water densities, at high



water densities, and at the critical point of water) was proposed [9]. Using limited ambient condition data, the method was applied to ϕ_2^{∞} at 1000 and 2000 K for CO₂, and at 1000 K for nonpolar CH₄ and polar substances H₂S, SO₂, and NH₃.

The goal of the present project is to systematically generalize the method of [9] for describing aqueous infinite-dilution fugacity coefficients over wide temperature and pressure ranges. The present work treats simple fluids, that is the noble gases (He, Ne, Ar, Kr, Xe, Rn), and compounds that are nearly spherical with dipole moments equal to or near zero (H₂, N₂, O₂, CO, CH₄).

The method treats both water and solutes as non-ionized species which places limits on the conditions of application. Both high temperature [19] and high pressure [20] cause dissociation and decomposition of water. Therefore, the upper temperature limit has been chosen as 2000 K, based on an *ab initio* investigation [19] of the H₂O-H₂ mixture that concluded "at 2000 K and below the mixture is almost fully molecular", though significant dissociation occurs at higher temperatures. The upper limit for the water density, ρ_1^* , is taken as 1500 kg m⁻³. While somewhat arbitrary, this limit is supported by the experimental observation that "at lower pressure (below approximately 12 GPa) liquid water has a predominantly molecular character" [20]. The corresponding maximum pressures increase from ~5.3 GPa at 500 K to ~7.7 GPa at 1000 K to ~9.7 GPa at 1500 K and to ~11.4 GPa at 2000 K. At temperatures below 500 K, the maximum ρ_1^* is determined by the *PT* coordinates of the melting curve of ice [21]. It increases from ~1250 kg m $^{-3}$ at 300 K to ~1350 kg m $^{-3}$ at 350 K and to ~1450 kg m⁻³ at 475 K. We also set a lower temperature limit of 298.15 K for applying the approach, as discussed below.

The work is organized as follows: first, we give Eq. (1) for calculating the fugacity coefficients of an infinitely dilute solute in water, ϕ_2^{∞} , through the density integration of the function A_{12}^{∞} defined in Eq. (2). As discussed previously [9], the values of A_{12}^{∞} for many classes of neutral solutes can reliably be estimated over wide ranges of temperature (298–2000 K) and water density (0–1500 kg m⁻³). The systematic application of such estimation methods to simple fluids is discussed in Section 2. In Section 3, the generated values of A_{12}^{∞} (298–2000 K, 0–1500 kg m⁻³) for each of the eleven solutes under consideration were fitted with Eq. (18), with correlated fugacity coefficients compared with literature data at supercritical (Section 3.2) and subcritical (Section 3.3) temperatures.

2. Theory

2.1. Fundamental relations

Since the proposed method for predicting thermodynamic properties of nonelectrolytes at infinite dilution in water has been thoroughly explained [9,10,15], only a brief outline will be given here. The basic equation for the calculation of ϕ_2^{∞} is an isothermal integration over density of the function A_{12}^{∞} [7].

$$\ln \phi_2^{\infty} = \int_{o}^{\rho_1} (A_{12}^{\infty} - 1) \frac{d\rho_1^*}{\rho_1^*} - \ln \frac{PV_1^*}{RT}$$
(1)

where

$$A_{12}^{\infty} = V_2^{\infty} / \kappa_T R T \tag{2}$$

with $\kappa_T = 1/\rho_1^*(\partial \rho_1^*/\partial P)_T$, the isothermal compressibility of pure solvent. Here, the subscript 2 refers to the solute and 1 to the solvent. Note that here and below ρ_1^* is in kg m⁻³ and V_1^* (the molar volume of pure water) and V_2^∞ are in cm³ mol⁻¹. The superscript ∞

denotes a property at infinite dilution, and * a pure-component property. The dimensionless quantity, A_{12}^{∞} is linearly related to the spatial integral of the molecular solute-water direct correlation function at infinite dilution [7] arising in Fluctuation Solution Theory [22,23]. Theoretically, A_{12}^{∞} is a smooth, continuous, and finite function at all conditions, including at the pure-solvent critical point, where the derivatives of the standard chemical potential of a solute diverge [24,25]. The critical A_{12}^{∞} is finite with a value that depends on the components [26] because the divergent V_2^{∞} is in the numerator and the divergent κ_T is in the denominator. For an ideal gas (IG), $A_{12}^{\infty} = 1$.

The current method predicts A_{12}^{∞} values at different temperatures and water densities, considering theoretical constraints wherever possible [9,15]. The initial departures from IG are linear in density

$$A_{12}^{\infty} = 1 + 2\rho_1^* B_{12} + \dots \tag{3}$$

where B_{12} is the temperature-dependent water-solute cross second virial coefficient [27,28]. At densities below ~950 kg m⁻³, A_{12}^{∞} is not a strong function of temperature [7]. At densities above ~950 kg m⁻³ at ambient temperatures and above ~450 kg m⁻³ at more than 1500 K, V_2^{∞} and, correspondingly, A_{12}^{∞} , can be predicted [9,15,29] on the basis of the theory of mixture of hard spheres that depends only on density [30]. An experimental value of V_2^{∞} at the standard state of 298.15 K and 0.1 MPa is needed to predict A_{12}^{∞} at high water densities. At the critical point of water, A_{12}^{∞} can be calculated from the value of the Krichevskii parameter [24], which is either known [31] or can be estimated [32] for many gases in water. References [24,25] define the Krichevskii parameter as the derivative $(\partial P/\partial x)_{V,T,x=0}^{c}$, at the critical point of a solvent. The Krichevskii parameter governs all the thermodynamic properties of dilute solutions in the neighborhood of the solvent critical point. At intermediate water densities, $500 < \rho_1^* < 900 \text{ kg m}^{-3}$, a variant of the corresponding-states principle was proposed for estimating A_{12}^{∞} [9,29]. After values of A_{12}^{∞} are available over the whole range of density, Equation (1) can be used to obtain ϕ_2^{∞} . The variation of A_{12}^{∞} is nonmonotonic at lower temperatures (<293 K) and pressures [29]. Though the observed low-temperature maximum disappears at pressures in excess of ~100 MPa, since our main interest is in high-temperature behavior, we concluded that accounting for this behavior would not be worthwhile. Thus, the low temperature limit of the correlation was set as 298.15 K.

2.2. Application to simple fluids

2.2.1. Second cross virial coefficients

Variations of B_{12} with *T* for interactions of water with many simple fluids (He, Ne, Ar, H₂, N₂, O₂, CO, CH₄) have been determined from accurate *ab initio* intermolecular potentials and available experimental data [33–39]. Such data have been fitted using polynomials of the type

$$B_{12}(T) = \sum_{i=1}^{4} a_i \left(\frac{T}{100}\right)^{b_i} \tag{4}$$

Parameters of Equation (4) for various simple fluids are given in Table 1. For water interactions with Kr, Xe, and Rn, values of B_{12} have been estimated as described in Ref. [40] and fitted with Equation (4). For CH₄-H₂O interactions, accurate B_{12} values are recommended in Ref. [36] up to 1000 K, these results were extrapolated to 2000 K by the method of [40] and fitted with Equation (4). The empirical method [40] is based on the application of the Tsonopoulos corresponding-states correlation [51] to 29 binary aqueous gas-water systems, which included nonpolar

Table 1	
Parameters of Equation (4) for calculating B_{12} in cm ³ mol ⁻¹ . The a_i are in cm ³ mol ⁻¹ .	

Gas	He ^a		Ne ^b		Ar ^b		Kr ^c		Xe ^c		Rn ^c	
i	a _i	b _i	a _i	b _i	ai	b _i	a _i	b _i	a _i	b _i	a _i	b _i
1	55.57	-0.347	45.8586	-0.30	96.1591	-0.31	308.36	-0.2	87.847	-0.1	101.91	-0.1
2	-59.25	-0.85	59.4400	-0.48	-211.074	-0.82	-333.91	-0.3	-182.245	-0.6	-235.28	-0.6
3	13.32	-1.45	-121.583	-0.69	-96.4425	-2.24	-408.10	-1.6	-659.674	-1.8	-1049.8	-1.9
4	-4.767	-2.1	-12.5141	-2.14	-12.6006	-4.60	-460.68	-3.5	-909.213	-3.8	-1571.9	-4.0
Gas	H_2^{d}		N ₂ ^e			0 ₂ ^f		CO ^g			CH ₄ ^h	
i	ai	bi	ai		bi	ai	bi	ai	bi		a _i	bi
1	33.047	-0.21	67.59	5	-0.24	124.605	-0.33	493.70	09 -0	.45	109.22	-0.2
2	-250.41	-1.50	-249	.83	-1.06	-214.421	-0.73	-579.	466 –0	.57	-202.52	-0.6
3	285.42	-2.26	-204	.38	-3.22	-102.818	-2.03	-248.	146 –2	.00	-235.86	-2.0
4	-186.78	-3.21	0		0	-22.360	-4.07	-271.	885 –4	.25	-297.63	-3.0

^a [33].

^b [34].

 c – our fit of B₁₂ values estimated as described in Ref. [40].

^d [35].

e [37].

^f [38].

^g [39].

^h Our fit of B_{12} at 298–1000 K [36] and at 1000–2000 K estimated as described in Ref. [40].

compounds (Ar, C₂H₄, *n*-alkanes up to *n*-octane, etc.), polar (CH₃Cl, HCl as examples) and hydrogen bonded compounds (alcohols, ammonia). It was shown that the mixture-specific parameter of Tsonopoulos correlation, k_{12} , after a small "size" correction, depends linearly on the Gibbs energy of hydration (Henry's constant in water) of a compound at 298 K and 0.1 MPa. The method [40] is used to estimate B_{12} for aqueous mixtures in the absence of experimental data.

2.2.2. Infinite-dilution partial molar volumes of simple fluids in water at 298.15 K

Based on the theory of mixtures of hard spheres [30], values V_2^{∞} for simple fluids in water at $T_r = 298.15$ K and $P_r = 0.1$ MPa can be used [9,29] to calculate thermodynamic properties at high water densities: at $\rho_1^* > 950$ at 400 K, $\rho_1^* > 900$ at 1000 K, and at $\rho_1^* > 450$ for $T \ge 1500$ K with the relation below

$$V_2^{\infty}(T,P) = V_2^{\infty}(T_r,P_r) \frac{\rho_1^*(T_r,P_r)}{\rho_1^*(T,P)}$$
(5)

All simple fluids are very poorly soluble in water at ambient conditions. As a consequence, V_2^{∞} values [41–49] of most of these gases in water at 298.15 K are known with significant uncertainties. For example, the V_2^{∞} data [49] at 298.15 and 303.15 K differs up to 4 cm³ mol⁻¹ (for O₂, Ar) and even 6 cm³ mol⁻¹ (for CH₄). The effects of the small temperature dependence of 298 and 303 K are unlikely to explain the differences, so they must arise from experimental error. In addition, the only experimental data point for Kr in water [44] is surprisingly close to V_2^{∞} of argon. Also, the data points for Xe [48] may be affected by formation of clathrates at the 33.4 MPa pressure of the measurements. Finally, no data are reported for Ne and Rn. The lack of complete measurements has required developing empirical estimates of V_2^{∞} for a number of simple fluids in water at 298.15 K and 0.1 MPa, as described below.

The reported results for Ar, H_2 , N_2 , O_2 , CO, and CH₄, for which there are consistent values from various research groups, were accepted. Also accepted, although with a larger uncertainty, was the reported value for He [49].

Several relations to correlate V_2^{∞} in water at 298.15 K and 0.1 MPa have been proposed in the literature. According to the corresponding-states principle (CSP) [50,51], results of V_2^{∞} //*c* vs. *T*/*T_c* for simple fluids should lie on a single curve, while variations for

other solute families will be different. As discussed in Ref. [44], V_2^{∞} varies approximately linearly with V_c , the critical volume of the pure solute. Fig. 1a confirms that observation with:

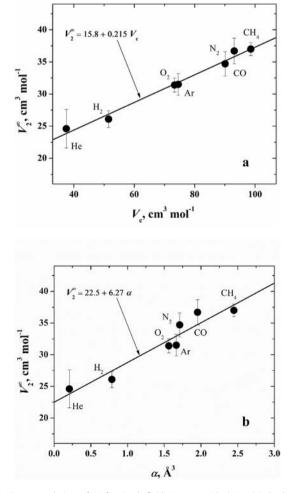


Fig. 1. Linear correlations of V_2^{∞} for simple fluids in water with a) V_c , critical volumes of pure gases, and with b) α , molecular polarizability of gases.

$$V_2^{\infty} = 15.8 + 0.215V_c \tag{6}$$

when all values are in $\text{cm}^3 \text{ mol}^{-1}$. Note that for "quantum gases" He, Ne, and H₂ the so-called "classical" values of V_c have been used, as recommended for corresponding-states relations [51].

A correlation between V_2^{∞} and the molecular polarizability of a solute, α , has been suggested [52]. Fig. 1b indicates that relation is approximately linear:

$$V_2^{\infty} = 22.5 + 6.27\alpha \tag{7}$$

where the molecular polarizability is given in Å³ units.

The concept of an empty layer of thickness δ_{sph} devoid of water around a spherical nonpolar solute of van der Waals radius of r_{vdW} suggests the following approximation (*e.g.*, [30], [53])

$$V_2^{\infty} = \frac{4\pi}{3} \left(r_{\rm vdW} + \delta_{\rm sph} \right)^3 \tag{8}$$

The theory for mixtures of hard spheres [30] predicts that for small r_{vdW} , δ_{sph} is large and decreasing, converging to a constant value at large r_{vdW} . Fig. 2a confirms this behavior; among the several relations that equally well approximate the data, Equation (9) has been selected:

1.0

0.9

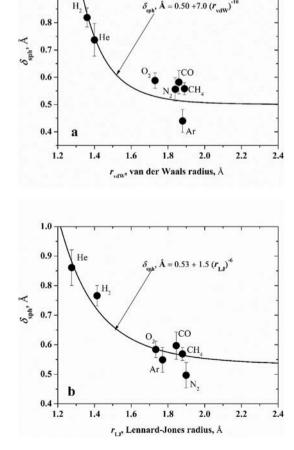


Fig. 2. Evaluation of δ_{sph} , the solute-solvent border thickness, from correlation of V_2^{∞} with the van der Waals (a) or Lennard-Jones (b) radii of solutes.

$$\delta_{sph} = 0.50 + 7.0 (r_{\rm vdW})^{-10} \tag{9}$$

where both δ_{sph} and r_{vdW} are given in Å units. The necessary values of r_{vdW} are taken from Refs. [54,55]. A final proposed measure of molecular size in solution is the radius given by the Lennard-Jones intermolecular potential model, r_{IJ} . Our correlation for this form is

$$\delta_{sph} = 0.53 + 1.50 (r_{\rm LJ})^{-6} \tag{10}$$

where both δ_{sph} and r_{LI} are given in Å units.

The results from all of these models are presented in Table 2. No compelling argument favors one method over the others, so all proposed relations have been employed as listed in the ninth column of Table 2. The average of values from Equations (7) to 10), listed in the tenth column of Table 2, have been used in subsequent calculations.

2.2.3. Values of the Krichevskii parameter and vapor-liquid distribution coefficients of simple fluids in water

Values of the A_{12}^{∞} at the critical point of water can be calculated with the relation [56]:

$$A_{12}^{\infty}\left(T_{c},\rho_{1,c}^{*}\right) = A_{Kr}\frac{V_{1,c}^{*}}{RT_{c}}$$
(11)

where $V_{1,c}^*$ is the critical molar volume of water, and A_{Kr} is the (constant) Krichevskii parameter [24,57]. For most simple fluids in water, values of A_{Kr} are known with high precision [31], mainly from high-temperature values of solute distribution between equilibrium vapor and liquid phases of water [58].

The distribution coefficient is defined as $K_D = \lim_{x \to \infty} y/x$, where y and x are the mole fractions of solute in the coexisting vapor and liquid phases, respectively. At the solvent's critical point, where both phases are identical, K_D is unity. Expanding the chemical potential of a solute about the solvent's critical point, reveals a theoretical relation for the temperature dependence of K_D at near-critical conditions [59]

$$RT \ln K_D = 2A_{Kr} \cdot \frac{\left[\rho_{1,L}^* - \rho_{1,c}^*\right]}{\left(\rho_{1,c}^*\right)^2}$$
(12)

where *L* designates the liquid phase of water. In Eq. (12) the proper dimension of density is in mol cm⁻³, with $\rho_{1,c}^* = 0.017874 \text{ mol cm}^{-3}$. Analysis of available data shows that Equation (12) is valid not only close to the critical point, but is also reliable as much as 150 K below water's critical temperature, $T_c = 647.096 \text{ K}$ [58]. In order to obtain K_D values at from 298.15 to T_c , we applied a temperature function to Equation (12), similar to that proposed in Ref. [60]:

$$RTlnK_{D} = 2A_{Kr} \frac{\left\lfloor \rho_{1,L}^{*} - \rho_{1,c}^{*} \right\rfloor}{\left(\rho_{1,c}^{*}\right)^{2}} \left(1 + a_{1}\tau + a_{2}\tau^{1.5} + a_{3}\tau^{2} + a_{4}\tau^{2.5}\right)$$
(13)

where $\tau = 1 - T/T_c$. The parameters of Equation (13) are given in Table 3. For all solutes except Rn, values of A_{Kr} are taken from Ref. [31], and K_D values are from the recommendations of [58]. For Rn, for which no experimental high-temperature data exist, A_{Kr} has been estimated from the Gibbs energy of hydration at 298.15 K, as proposed in Ref. [32]. Estimation of K_D has been made as described in Ref. [61]: first, data for the enthalpy of hydration and

Table 2
Values of V_2^{∞} simple fluids at 298.15 K, 0.1 MPa, see text.

Solute	$V_2^{\infty}(experimental)$ cm ³ mol ⁻¹	Method ^a	V_2^{∞} (selected), cm ³ mol ⁻¹	r _{vdW} , Å	r _{LJ} , Å	V_c , cm ³ mol ⁻¹	α, Å ³	Estimated V_2^{∞} , cm ³ mol ⁻¹	Accepted V_2^{∞} , cm ³ mol ⁻¹
He Ne	24.6 ^b	Vibr	24.6 ± 3.0 ^c	1.40 ^d 1.54 ^d	1.28 ^e 1.41 ^e	37.5 ^{e,f} 40.3 ^{e,f}	0.208 ^g 0.381 ^g	24.5 (Eq. (6)) 24.9 (Eq. (7)) 24.5 (Eq. (9)) 24.4 (Eq. (10))	24.6
Ar	32.7 ^b 31.0 ^h 29.4 ⁱ 32.6 ^k 31.71 ¹	Vibr MF Pycn Vibr Dilat	31.5 ± 1.7 ^m	1.88 ^d	1.77 ^e	74.57 ^e	1.664 ^g		
Kr	32.8 ^k	Vibr		2.02 ^d	1.83 ^e	91.20 ^e	2.498 ^g	35.4 (Eq. (6)) 38.4 (Eq. (7)) 40.7 (Eq. (9)) 34.8 (Eq. (10))	37.3
Xe	42.7 ⁿ	Vibr		2.16 ^d	2.02 ^e	118.0 ^e	4.005 ^g		45.0
Rn				2.20 °		140.0 ^e	~4.8 ^p	45.9 (Eq. (6)) 52.4 (Eq. (7)) 49.8 (Eq. (9))	49.4
H ₂	23.1 ^b 26.7 ^k 25.20 ¹ 26 ^q	Vibr Vibr Dilat Dilat	26.1 ± 1.3 [°]	1.36 ^{s,t}	1.41 ^e	51.5 ^{e,f}	0.787 ^g	45.0 (Eq. (5))	
N ₂	33.1 b 35.5 i 34.3 h 35.7 k 40 q.u	Vibr Pycn MF Vibr Dilat	34.7 ± 1.9 ^m	1.84 ^v	1.90 ^e	90.10 ^e	1.710 ^g		
02	32.1 b 30.6 i 31.1 h 33.2 k 30.38 l 31.9 q	Vibr Pycn MF Vibr Dilat Dilat	31.4 ± 1.1 ^m	1.73 ^v	1.73 ^e	73.37 ^e	1.562 ^g		
со	37.3 ^k 36 ^q	Vibr Dilat	36.7 \pm 2.0 ^c	1.86 ^v	1.85 ^e	93.1 ^e	1.953 ^g		
CH4	32.0 b,u 36.8 w 34.5 k,u 37.42 l 36.3 × 37 ^q	Vibr Vibr Vibr Dilat Dilat Dilat	37.0 ± 1.0 ^m	1.89 ^v	1.88 ^e	98.6 ^e	2.448 ^g		

^a Methods: Vibr – Vibrating tube; MF – Magnetic Float; Pycn – Pycnometer; Dilat – Dilatometer.

^b [49].

^c Our estimate of uncertainty.

^d [54].

^e [51].

f "Classical value", different for quantum fluids from measured values (57.3 for He, 41.70 for Ne, 64.2 for H₂).

^g Computational Chemistry Comparison and Benchmark DataBase of NIST at http://cccbdb.nist.gov/exp2x.asp.

- h [45].
- i [46].
- ^k [44. ¹ [43].
- ^m the uncertainty for the confidence level of 0.95.
- n [48], P = 33.41 MPa, i.e. the field of stability of a clathrate.
- ° [55].

^p The online table of Schwerdtfeger P. at http://ctcp.massey.ac.nz/Tablepol2017.pdf.

^q [41]. r

- as selected in Ref. [10]. s
- Calculated from the r_{vdW} for an atom and the bond distance *l* for diatomic molecule as explained in Ref. [54]. $r_{vdW} = 1.20 \text{ Å}$ [54] and l = 0.741 Åt
- ^u not used as an outlier.
- ^v calculated from the van der Waals volume of a molecule [54].
- ^w [47], *P* is between 28 and 35 MPa.
- ^x [42].

Table 3

Parameters of Equation (13) for the temperature dependence of K_D , including values of the Krichevskii parameter.

Solute	A _{Kr} , MPa	<i>a</i> ₁	<i>a</i> ₂	<i>a</i> ₃	a_4
He	169 ^a	-0.64158	2.6892	-4.7045	2.8472
Ne	186 ^a	0.89014	-5.2142	7.3096	-3.1790
Ar	172 ^a	2.1975	-11.567	18.343	-9.7146
Kr	169 ^a	3.2541	-16.669	26.307	-13.870
Xe	150 ^a	-0.77542	3.2312	-3.7738	0.68247
Rn	143 ^b	-4.0737	12.064	-9.2242	0
H ₂	170 ^a	-2.1784	9.9059	-16.433	9.0854
N ₂	178 ^a	0.36979	-2.7266	4.7343	-2.8881
02	171 ^a	0.23481	-1.9722	3.3344	-2.0638
CO	174 ^a	2.5753	-13.013	20.252	-10.535
CH4	164 ^a	0.0	-0.49212	1.2971	-1.2985

^a [31, including errata].

^b [32].

the heat capacity of hydration of Rn in water at 298.15 K [62] allowed prediction of the Gibbs energies of hydration of Rn up to 473 K. These were converted into $k_{\rm H}$ values for Rn in the mole fraction scale. Then, vapor phase fugacity coefficients of Rn at infinite dilution in the aqueous vapor (*V*) phase, $\phi_{2,V}^{\infty}$, were calculated using B_{12} from Equation (4), leading to values of K_D found from $K_D = k_{\rm H}/(P_{1,s}^*\phi_{2,V}^\infty)$, where $P_{1,s}^*$ is the water saturation pressure. Finally, estimated values of $A_{\rm Kr}$ and K_D were fitted to Equation (13). The accuracy of our high-temperature results for Rn is not as good as for other gases, where K_D values are reliable to within a few percent for T > 400 K and are much more accurate for T < 400 K.

2.2.4. Estimation of A_{12}^{∞} values at densities of water between 500 and 900 kg m⁻³

We have shown [9,29] that corresponding-states relations exist for the reduced A_{12}^{∞} function, $A_{12, red}^{\infty}$, defined as

$$A_{12,red}^{\infty} = \frac{A_{12}^{\infty}(T,\rho_1^*)}{A_{12}^{\infty}(T_r,\rho_{1,r}^*)}$$
(14)

where properties with the subscript r refer to 298.15 K and 0.1 MPa. Values of $A_{12, red}^{\infty}$ are quite similar within many classes of organic compounds (alcohols, amines, etc.) in water [9]. At specified conditions, the values of $A_{12,red}^{\infty}$ decrease from simple fluids to normal fluids to polar compounds to hydroxides [9,29]. Data-based values of $A_{12, red}^{\infty}$ are available up to 700 K. The extrapolation of $A_{12, red}^{\infty}$ to higher temperatures is based on the observation [9], following from the theory of mixtures of hard spheres [30], that the hightemperature limit of $A_{12, red}^{\infty}$ is equal to $A_{11, red}^{*}$, where $A_{11, red}^{*} =$ $\frac{A_{11}^*(T,\rho_1^*)}{A_{11}^*(T,\rho_{1,r}^*)}$ with the reduced bulk modulus, $A_{11}^* = \frac{V_1^*}{\kappa_T R T}$. Since $A_{11, red}^*$ is known with high precision up to very high T and P from an accurate water EoS [63], $A_{12, red}^{\infty}$ values are also known at T > 1200 K at moderate and high water densities. Note that while the IAPWS-95 EoS for water [63] was recommended only to 1273 K and 1 GPa, its authors stated that "IAPWS-95 can be extrapolated up to extremely high pressures and temperatures", giving us confidence that the properties up to 2000 K and 10 GPa are reliable. Combining experimental data at moderate temperatures and water densities with the known high-temperature limits, estimates of $A_{12, red}^{\infty}$ were made for several classes of solutes, including simple fluids, at water densities between 500 and 900 kg m^{-3} and temperatures from 600 K to 2000 K [9].

To extend the correlation for $A_{12, red}^{\infty}$ to ambient temperatures, high precision data for K_D can be used in the following way. Values of K_D can be obtained using Equation (1) for the liquid (*L*) and for

the vapor (V) phases of water.

$$\ln K_D = \ln \frac{\phi_{2,L}^{\infty}}{\phi_{2,V}^{\infty}} = \int_{\rho_{1,V}^*}^{\rho_{1,L}} (A_{12}^{\infty} - 1) \frac{d\rho_1^*}{\rho_1^*}$$
(15)

Matching calculated and experimental K_D values constrains the variation of A_{12}^{∞} between the densities of coexisting vapor and liquid phases of water, which are not observable because they are in the metastable or unstable two-phase range.

This allows the use of two sources of information about $A_{12, red}^{\infty}$ of simple fluids at moderate water densities: 1) the precise experimental data on V_2^{∞} for CH₄ [47], together with the somewhat less accurate V_2^{∞} values for Ar [48] up to 700 K (the values at rounded water densities, obtained by interpolation of experimental data, are shown as stars in Fig. 3); and 2) values obtained by imposing agreement between experiment and values of K_D calculated from Equation (15) for Ar, chosen as the basis (values of $A_{12, red}^{\infty}$, estimated in this way, are shown as yellow circles in Fig. 3). The results from the various sources are shown in Fig. 3 with different symbols denoting the sources of the values. These data for $A_{12, red}^{\infty}$ from 298 to 2000 K at water densities of 500, 600, 700, 800 and 900 kg m⁻³ have been correlated as

$$A_{12,red}^{\infty} = a + bT + cT^2 \tag{16}$$

with the parameters *a*, *b*, and *c* given in Table 4.

2.3. Evaluation of the isothermal course of A_{12}^{∞} at various water densities

The above methods have been used to estimate A_{12}^{∞} as a function of *T* and ρ_1^* . A convenient representation for interpolation and smoothing of isothermal variations with water density is the function [9,15].

$$\ell = (A_{12}^{\infty} - 1) / \rho_1^* \tag{17}$$

which has a smaller range of variations compared to A_{12}^{∞} . At $\rho_1^* = 0$ Equation (3) gives *Y* equal to $2B_{12}$, providing a high-precision intercept for *Y*. Estimated values of *Y*, as discussed above, are available at $\rho_1^* \ge 500 \text{ kg m}^{-3}$, and at near-critical temperatures and the critical density, through the Krichevskii parameter. Over the density range of $100-400 \text{ kg m}^{-3}$, we have no independent

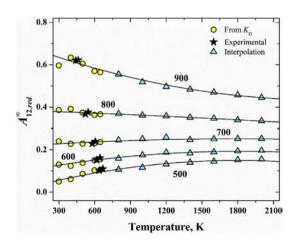


Fig. 3. Values $A_{12,red}^{\infty}$ for simple fluids in water from various sources of information. Curves are calculated with Equation (16) using parameters in Table 4. Numbers (500, ..., 900) designate water densities in kg m⁻³.

 Table 4

 Parameters of Equation (16) at different water densities.

$\rho_1^*,\mathrm{kg}\;\mathrm{m}^{-3}$	а	$10^4 b$, K ⁻¹	$10^8 c$, K ⁻²
500	0.0147	1.512	-4.223
600	0.0987	10.42	-2.873
700	0.2179	3.796	-1.058
800	0.3849	-0.205	-0.249
900	0.6933	-2.074	4.145

estimates of A_{12}^{∞} , however, as experience shows, the contribution of this region to the integral for the fugacity coefficient, Eq. (1), is important. Therefore, over the density range of 100–400 kg m⁻³ we varied *Y* values to smoothly join the points between ρ_1^* equal to 0 and 500 kg m⁻³, forming a convex function. The properly selected A_{12}^{∞} give at their integration, see Eq. (15), a good agreement with experimental values of $K_{\rm D}$. Such a procedure was especially important for reliability when T < 500 K.

Fig. 4 shows *Y* for He and Xe in water at three temperatures: 298.15, 647.1 ($\approx T_c$), and 2000 K. The values at $\rho_1^* = 0$, have been calculated from B_{12} values from Eq. (4), with parameters from Table 1. The star at the critical temperature T_c and critical density has been calculated from Eq. (11) using A_{Kr} values in Table 3. The circles for $\rho_1^* = 500-900 \text{ kg m}^{-3}$ were calculated as described in Section 2.2.4 by using Eq. (16) to obtain $A_{12,red}^{\infty}$, and Eq. (14) to convert results to A_{12}^{∞} with V_2^{∞} at 298.15 K, 0.1 MPa from Table 2, while those for $\rho_1^* \ge 1000 \text{ kg m}^{-3}$ have been obtained from the hard-sphere relations of Section 2.2.2, Eq. (5), with V_2^{∞} at 298.15 K,

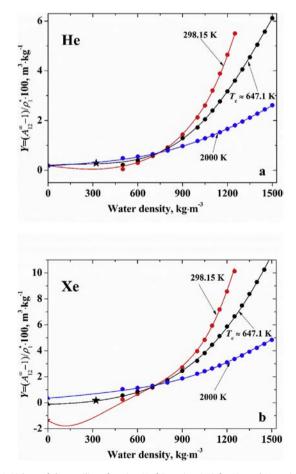


Fig. 4. Values of the auxiliary function Y of Equation (17) for He and Xe at infinite dilution in water at 298.15, 647.1, and 2000 K.

0.1 MPa from Table 2. Note that there are Y values along the 298.15 K isotherm at densities where two phases coexist, so these values are for metastable and unstable conditions. This is similar to the van der Waals loop for pure-component vapor-liquid equilibria from an EoS. The variation shown is required to reproduce experimental K_D values at 298.15 K. The lines in Fig. 4 are from the global formula described below.

3. Results and discussion

3.1. Global fit of results

Tabulation of A_{12}^{∞} estimates was made for more 700 conditions for each solute for 13 temperatures between 298.15 and 623.15 K with a step of 25 K; at 633.15, 643.15, 647.10, 673.15 K; for nine temperatures between 700 and 1500 K with a step of 100 K; and at 1700 and 2000 K. The data were fitted with the function

$$A_{12}^{\infty} = 1 + \rho_1^* \left[a_0 + a_1 \rho_1^* + a_2 (\rho_1^*)^2 + a_3 (\rho_1^*)^3 + a_4 (\rho_1^*)^4 + a_5 (\rho_1^*)^6 \right]$$
(18)

where

$$a_0 = 2\Omega B_{12} \tag{19}$$

with $\Omega = \frac{10^{-3}}{M_{y}} \approx 55.508 \cdot 10^{-6}$ to convert B_{12} volume units of cm³ mol⁻¹ to m³ kg⁻¹. The other temperature-dependent coefficients are

$$a_i = \sum_{n=1}^7 a_{in} T_r^{-n}$$
(20)

where $T_r = T/T_c$ with $T_c = 647.096$ K [63]. For example, $a_1 = a_{11}T_r^{-1} + a_{12}T_r^{-2} + a_{13}T_r^{-3} + a_{14}T_r^{-4} + a_{15}T_r^{-5} + a_{16}T_r^{-6} + a_{17}T_r^{-7}$. An equation similar to Eq. (18) was used in Refs. [9,10], but without the a_4 term. It was found that addition of this term decreased the sum of squared errors by about 20–30%. Table 5 give the values of the a_{in} .

Evaluating Equation (1) gives infinite-dilution fugacity coefficients of solute (2) in solvent (1)

$$\ln \phi_{2}^{\infty} = \rho_{1}^{*} \left[a_{o} + \frac{a_{1}}{2} \rho_{1}^{*} + \frac{a_{2}}{3} (\rho_{1}^{*})^{2} + \frac{a_{3}}{4} (\rho_{1}^{*})^{3} + \frac{a_{4}}{5} (\rho_{1}^{*})^{4} + \frac{a_{5}}{7} (\rho_{1}^{*})^{6} \right] - \ln \frac{PV_{1}^{*}}{RT},$$
(21)

where ρ_1^* is in kg m⁻³ and V_1^* is in cm³ mol⁻¹.

3.2. Comparison with literature data at supercritical temperatures

3.2.1. Infinite-dilution fugacity coefficients

Fig. 5 (for T = 750 K) and Fig. 6 (for T = 1500 K) compare values of ϕ_2^{∞} from the presented method with those from three literature EoS: computer-simulation generated *PVTX* properties of binary water-gas systems (SUPERFLUID [11]), and [12], and a perturbationtheory EoS [13]. Figs. S1 and S2 of the Supplementary Materials show corresponding graphs for 1000 and 2000 K. Generally, results of all works are in reasonable agreement, although they are based on various computational approaches. Note that the EoS of [13] is not recommended for conditions of T < 750 K and P < 50 MPa; and SUPERFLUID EoS [11] for Ar and N₂ should not be used for P < 500 MPa. Our values at low supercritical temperatures are

Table 5
Parameters of Eq. (20) for different solutes.

$i n \rightarrow \downarrow$	1	2	3	4	5	6	7
+ He							
1	$0.330171 \cdot 10^{-4}$	$-0.956234 \cdot 10^{-4}$	$1.66334 \cdot 10^{-4}$	$-1.64667 \cdot 10^{-4}$	$0.835003 \cdot 10^{-4}$	$-2.05151 \cdot 10^{-5}$	$1.96847 \cdot 10^{-6}$
2	$0.168282 \cdot 10^{-7}$	$-0.134021 \cdot 10^{-6}$	0.162366 • 10 ⁻⁶	$-0.0632820 \cdot 10^{-6}$	0.111715 · 10 ⁻⁷	$-0.0342337 \cdot 10^{-7}$	0.0731267.10-8
3	$0.296736 \cdot 10^{-10}$	$0.0354800 \cdot 10^{-9}$	$-0.115563 \cdot 10^{-9}$	$0.0630922 \cdot 10^{-9}$	$-0.00984355 \cdot 10^{-9}$	$0.00413077 \cdot 10^{-10}$	0
4	$-0.228315 \cdot 10^{-13}$	$0.0724047 \cdot 10^{-12}$	$-0.0251653 \cdot 10^{-12}$	0	$-0.0470755 \cdot 10^{-13}$	$0.283931 \cdot 10^{-14}$	$-0.485251 \cdot 10^{-1}$
5	$0.290321 \cdot 10^{-20}$	$-1.64964 \cdot 10^{-20}$	$1.08055 \cdot 10^{-20}$	$-1.41333 \cdot 10^{-21}$	0	0	0
Ne							
1	$0.272235 \cdot 10^{-4}$	$-0.990487 \cdot 10^{-4}$	$1.07231 \cdot 10^{-4}$	$-0.527256 \cdot 10^{-4}$	$0.215489 \cdot 10^{-4}$	$-0.977109 \cdot 10^{-5}$	$2.02335 \cdot 10^{-6}$
2	$0.146673 \cdot 10^{-7}$	$-0.0307540 \cdot 10^{-6}$	$0.374800 \cdot 10^{-6}$	$-0.573740 \cdot 10^{-6}$	3.19327 • 10 ⁻⁷	$-0.687621 \cdot 10^{-7}$	$0.364859 \cdot 10^{-8}$
3	$0.488631 \cdot 10^{-10}$	$-0.208907 \cdot 10^{-9}$	$-0.132675 \cdot 10^{-9}$	$0.414531 \cdot 10^{-9}$	$-0.232656 \cdot 10^{-9}$	$0.406685 \cdot 10^{-10}$	0
4 5	$-0.318303 \cdot 10^{-13}$ $0.0843029 \cdot 10^{-20}$	$0.207455 \cdot 10^{-12}$ -1.53649 \cdot 10^{-20}	$-0.126351 \cdot 10^{-12}$ $0.846021 \cdot 10^{-20}$	$0 \\ -0.444989 \cdot 10^{-21}$	$0.0192703 \cdot 10^{-13}$	$0.8040190 \cdot 10^{-14}$	$-2.40858 \cdot 10^{-15}$
	0.0845029+10	-1.55649+10	0.840021.10	-0.444989+10	0	0	0
Ar	4					5	6
1	$3.31120 \cdot 10^{-4}$	$-16.9690 \cdot 10^{-4}$	$34.2329 \cdot 10^{-4}$	$-34.5364 \cdot 10^{-4}$	$18.5501 \cdot 10^{-4}$	$-50.9746 \cdot 10^{-5}$	$56.4098 \cdot 10^{-6}$
2	$-6.38608 \cdot 10^{-7}$	$3.26991 \cdot 10^{-6}$	$-6.28720 \cdot 10^{-6}$	$5.93872 \cdot 10^{-6}$	$-29.5699 \cdot 10^{-7}$	$7.49049 \cdot 10^{-7}$	$-7.55633 \cdot 10^{-8}$
3	$5.22779 \cdot 10^{-10}$ -1.57202 \cdot 10^{-13}	$-2.26188 \cdot 10^{-9}$ $0.605600 \cdot 10^{-12}$	$3.54594 \cdot 10^{-9}$ -0.562860 \cdot 10^{-12}	$-2.59097 \cdot 10^{-9}$	$0.902573 \cdot 10^{-9}$ $2.46531 \cdot 10^{-13}$	$-1.24931 \cdot 10^{-10}$ $-12.3992 \cdot 10^{-14}$	0 19.9139∙10 ⁻¹⁵
4 5	$-1.57202 \cdot 10$ $1.10779 \cdot 10^{-20}$	$-4.96735 \cdot 10^{-20}$	$-0.562860 \cdot 10$ 4.68195 \cdot 10 ⁻²⁰	$0 \\ -12.5029 \cdot 10^{-21}$	2.46531.10	-12.3992•10 0	0
Kr							
1	$3.37502 \cdot 10^{-4}$	$-18.0856 \cdot 10^{-4}$	37.8160 · 10 ⁻⁴	$-38.9855 \cdot 10^{-4}$	$21.0871 \cdot 10^{-4}$	$-57.5198 \cdot 10^{-5}$	$62.4522 \cdot 10^{-6}$
2	$-5.89268 \cdot 10^{-7}$	$3.45089 \cdot 10^{-6}$	$-7.26941 \cdot 10^{-6}$	$7.27048 \cdot 10^{-6}$	$-37.0316 \cdot 10^{-7}$	9.23612 · 10 ⁻⁷	$-8.83522 \cdot 10^{-8}$
3	$3.15911 \cdot 10^{-10}$	$-1.92919 \cdot 10^{-9}$	3.93134·10 ⁻⁹	$-3.52677 \cdot 10^{-9}$	$1.43707 \cdot 10^{-9}$	$-2.18517 \cdot 10^{-10}$	0
4	$0.227397 \cdot 10^{-13}$	$0.136816 \cdot 10^{-12}$	$-0.255015 \cdot 10^{-12}$	0	$2.35063 \cdot 10^{-13}$	$-15.1326 \cdot 10^{-14}$	$28.2990 \cdot 10^{-15}$
5	$-1.48330 \cdot 10^{-20}$	2.42315 • 10 ⁻²⁰	$-1.61166 \cdot 10^{-20}$	$4.71965 \cdot 10^{-21}$	0	0	0
Xe							
1	$2.46371 \cdot 10^{-4}$	$-14.2013 \cdot 10^{-4}$	$32.3087 \cdot 10^{-4}$	$-35.7220 \cdot 10^{-4}$	20.1886 • 10 ⁻⁴	$-56.5366 \cdot 10^{-5}$	$62.4672 \cdot 10^{-6}$
2	$-2.59311 \cdot 10^{-7}$	$2.31057 \cdot 10^{-6}$	$-6.14630 \cdot 10^{-6}$	$7.10728 \cdot 10^{-6}$	$-38.8621 \cdot 10^{-7}$	$9.95998 \cdot 10^{-7}$	$-9.55320 \cdot 10^{-8}$
3	$-0.659378 \cdot 10^{-10}$	$-0.662369 \cdot 10^{-9}$	$2.91966 \cdot 10^{-9}$	$-3.67398 \cdot 10^{-9}$	$1.73832 \cdot 10^{-9}$	$-2.81519 \cdot 10^{-10}$	0
4 5	$1.98125 \cdot 10^{-13} \\ -2.96836 \cdot 10^{-20}$	$-0.453872 \cdot 10^{-12} \\ 8.00940 \cdot 10^{-20}$	$\begin{array}{r} 0.241266 \cdot 10^{-12} \\ -7.34314 \cdot 10^{-20} \end{array}$	0 19.0536 • 10 ⁻²¹	$1.75538 \cdot 10^{-13}$	$-15.7832 \cdot 10^{-14}$ 0	33.5822 • 10 ⁻¹⁵ 0
Rn	200000 10						
1	$2.29992 \cdot 10^{-4}$	$-16.5568 \cdot 10^{-4}$	$44.6590 \cdot 10^{-4}$	$-57.1003 \cdot 10^{-4}$	37.1623 • 10 ⁻⁴	$-119.633 \cdot 10^{-5}$	$151.402 \cdot 10^{-6}$
2	$-5.73390 \cdot 10^{-7}$	$4.51594 \cdot 10^{-6}$	$-11.2419 \cdot 10^{-6}$	13.0822 · 10 ⁻⁶	$-77.5109 \cdot 10^{-7}$	$22.7877 \cdot 10^{-7}$	$-26.3489 \cdot 10^{-8}$
3	5.91825 · 10 ⁻¹⁰	$-3.95159 \cdot 10^{-9}$	$7.84421 \cdot 10^{-9}$	$-6.92661 \cdot 10^{-9}$	2.80369 · 10 ⁻⁹	$-4.30147 \cdot 10^{-10}$	0
4	$-1.57576 \cdot 10^{-13}$	$1.08196 \cdot 10^{-12}$	$-1.30155 \cdot 10^{-12}$	0	8.63588 · 10 ⁻¹³	$-51.0940 \cdot 10^{-14}$	$91.6656 \cdot 10^{-15}$
5	$-0.0431787 \cdot 10^{-20}$	$-4.66333 \cdot 10^{-20}$	$5.66059 \cdot 10^{-20}$	$-17.4462 \cdot 10^{-21}$	0	0	0
H ₂							
1	$1.02969 \cdot 10^{-4}$	$-3.77391 \cdot 10^{-4}$	$5.15786 \cdot 10^{-4}$	$-3.10456 \cdot 10^{-4}$	$0.670948 \cdot 10^{-4}$	$0.581482 \cdot 10^{-5}$	$-3.01150 \cdot 10^{-6}$
2	$-1.51880 \cdot 10^{-7}$	$0.454209 \cdot 10^{-6}$	$-0.320341 \cdot 10^{-6}$	$-0.126678 \cdot 10^{-6}$	2.59977 · 10 ⁻⁷	$-1.164377 \cdot 10^{-7}$	$1.74266 \cdot 10^{-8}$
3	$2.25633 \cdot 10^{-10}$	$-0.614891 \cdot 10^{-9}$	$0.474883 \cdot 10^{-9}$	$-0.144575 \cdot 10^{-9}$	$0.0214011 \cdot 10^{-9}$	$-0.0229158 \cdot 10^{-10}$	0
4	$-1.06420 \cdot 10^{-13}$	$0.304710 \cdot 10^{-12}$	$-0.155026 \cdot 10^{-12}$	0	$-0.0232358 \cdot 10^{-13}$	$0.795336 \cdot 10^{-14}$	$-1.67248 \cdot 10^{-15}$
5	$1.18910 \cdot 10^{-20}$	$-4.03882 \cdot 10^{-20}$	$2.50264 \cdot 10^{-20}$	$-3.25879 \cdot 10^{-21}$	0	0	0
N ₂							
1	$1.71614 \cdot 10^{-4}$	$-7.87088 \cdot 10^{-4}$	$14.4505 \cdot 10^{-4}$	$-13.1668 \cdot 10^{-4}$	$6.31582 \cdot 10^{-4}$	$-15.4929 \cdot 10^{-5}$	$15.4923 \cdot 10^{-6}$
2	$-2.11747 \cdot 10^{-7}$	$1.05405 \cdot 10^{-6}$	$-1.87483 \cdot 10^{-6}$	$1.55157 \cdot 10^{-6}$	$-6.40910 \cdot 10^{-7}$	$1.32852 \cdot 10^{-7}$	$-1.15412 \cdot 10^{-8}$
3 4	$1.63879 \cdot 10^{-10} \\ -0.439095 \cdot 10^{-13}$	$-0.636905 \cdot 10^{-9}$ $0.204020 \cdot 10^{-12}$	$0.858253 \cdot 10^{-9}$ -0.162376 \cdot 10^{-12}	$-0.486214 \cdot 10^{-9}$	$0.100180 \cdot 10^{-9}$ $0.427314 \cdot 10^{-13}$	$\begin{array}{r} -0.0328645 \!\cdot\! 10^{-10} \\ -1.24034 \!\cdot\! 10^{-14} \end{array}$	0 0.473523 • 10 ⁻¹⁵
4 5	$-0.439093 \cdot 10^{-20}$ $0.270801 \cdot 10^{-20}$	$-2.12050 \cdot 10^{-20}$	$1.73572 \cdot 10^{-20}$	$-3.34712 \cdot 10^{-21}$	0.427514.10	-1.24034•10 0	0.475525+10
02							
1	$1.14609 \cdot 10^{-4}$	$-4.78505 \cdot 10^{-4}$	$8.15298 \cdot 10^{-4}$	$-6.79959 \cdot 10^{-4}$	$2.83409 \cdot 10^{-4}$	$-5.55452 \cdot 10^{-5}$	3.85476 • 10 ⁻⁶
2	$-0.995565 \cdot 10^{-7}$	0.418916 • 10 ⁻⁶	$-0.665720 \cdot 10^{-6}$	$0.465682 \cdot 10^{-6}$	$-1.17181 \cdot 10^{-7}$	$-0.0324792 \cdot 10^{-7}$	$0.364776 \cdot 10^{-8}$
3	$0.742646 \cdot 10^{-10}$	$-0.168799 \cdot 10^{-9}$	$0.132150 \cdot 10^{-9}$	$-0.0453310 \cdot 10^{-9}$	$-0.00489050 \cdot 10^{-9}$	$0.0424158 \cdot 10^{-10}$	0
4	$-0.160987 \cdot 10^{-13}$	$0.0654708 \cdot 10^{-12}$	$-0.0108608 \cdot 10^{-12}$	0	$-0.210736 \cdot 10^{-13}$	$1.41196 \cdot 10^{-14}$	$-2.73644 \cdot 10^{-12}$
5	$0.0811105 \cdot 10^{-20}$	$-1.09479 \cdot 10^{-20}$	0.470839 • 10 ⁻²⁰	0.960803 • 10 ⁻²¹	0	0	0
CO							
1	$2.98880 \cdot 10^{-4}$	$-15.5113 \cdot 10^{-4}$	31.4220 · 10 ⁻⁴	$-31.4446 \cdot 10^{-4}$	$16.4808 \cdot 10^{-4}$	$-43.4599 \cdot 10^{-5}$	$45.4478 \cdot 10^{-6}$
2	$-4.58140 \cdot 10^{-7}$	$2.51278 \cdot 10^{-6}$	$-4.97136 \cdot 10^{-6}$	$4.69613 \cdot 10^{-6}$	$-22.6036 \cdot 10^{-7}$	$5.31538 \cdot 10^{-7}$	$-4.72948 \cdot 10^{-8}$
3	$3.07899 \cdot 10^{-10}$	$-1.43490 \cdot 10^{-9}$	$2.38664 \cdot 10^{-9}$	$-1.83690 \cdot 10^{-9}$	$0.666573 \cdot 10^{-9}$	$-0.939165 \cdot 10^{-10}$	0
4	$-0.654523 \cdot 10^{-13}$ $0.388032 \cdot 10^{-20}$	$\begin{array}{r} 0.303023 \cdot 10^{-12} \\ -2.63707 \cdot 10^{-20} \end{array}$	$-0.274778 \cdot 10^{-12}$ 2.35466 \cdot 10^{-20}	$0 \\ -4.84078 \cdot 10^{-21}$	1.08504•10 ⁻¹³ 0	$-5.24611 \cdot 10^{-14}$ 0	8.04952 • 10 ⁻¹⁵ 0
5							

Table 5 (continued)

	continueu y						
$i n \rightarrow$	1	2	3	4	5	6	7
+							
CH ₄							
1	$2.97057 \cdot 10^{-4}$	$-16.1247 \cdot 10^{-4}$	$34.4063 \cdot 10^{-4}$	$-36.0221 \cdot 10^{-4}$	$19.5874 \cdot 10^{-4}$	$-53.2147 \cdot 10^{-5}$	57.0850 • 10 ⁻⁶
2	$-4.49849 \cdot 10^{-7}$	$2.93254 \cdot 10^{-6}$	$-6.71023 \cdot 10^{-6}$	$7.07104 \cdot 10^{-6}$	$-36.8944 \cdot 10^{-7}$	$9.22213 \cdot 10^{-7}$	$-8.66110 \cdot 10^{-8}$
3	$1.61007 \cdot 10^{-10}$	$-1.37627 \cdot 10^{-9}$	3.44496 • 10 ⁻⁹	$-3.48885 \cdot 10^{-9}$	$1.51742 \cdot 10^{-9}$	$-2.38812 \cdot 10^{-10}$	0
4	$0.766418 \cdot 10^{-13}$	$-0.0700448 \cdot 10^{-12}$	$-0.0767257 \cdot 10^{-12}$	0	$1.97840 \cdot 10^{-13}$	$-14.2101 \cdot 10^{-14}$	$28.0351 \cdot 10^{-15}$
5	$-1.50262 \cdot 10^{-20}$	$3.06667 \cdot 10^{-20}$	$-2.51644 \cdot 10^{-20}$	$6.99891 \cdot 10^{-21}$	0	0	0

closest to those of [13], while at the highest temperature, 2000 K, our results usually are higher than all literature EoS. This would lead to lower concentrations than from other models at the same conditions. Generally, high-temperature thermodynamic properties of simple fluids at high dilution in water appears to be reasonably well constrained by consistent results of several studies, including the current one: at densities above 1000 K the agreement of various EoS is usually within 1 log₁₀ unit, which likely reflects the uncertainty of high-density predictions. In the absence of precise experimental results at supercritical temperatures, a more definite conclusion is not warranted.

3.3. Comparison with literature data at subcritical temperatures

Data on the properties of dilute solutions of simple fluids in water at subcritical temperatures are known with high precision, especially at temperatures below 373 K. For example, see recommendations on values of $k_{\rm H}$ and $K_{\rm D}$ by Fernández-Prini et al. [58]. This section compares our results with these recommendations.

3.3.1. Comparisons of K_D and introduction of reference K_D values

As discussed in Section 2.2.4, Equation (15) allows the calculation of K_D from the "volumetric" information

$$\ln K_{\rm D} = \ln \phi_{2,L}^{\infty} - \ln \phi_{2,V}^{\infty} \tag{22}$$

where *L* and *V* designate the coexisting liquid and vapor phases of water. Fig. 7 shows comparisons of the recommended values of lnK_D [58] with those calculated from Equation (22). In all cases, the difference is less than 0.11 ln units (less than 0.05 log_{10} units) or 11%. Unfortunately, this accuracy in K_D is not within the experimental uncertainty of 1% at temperatures below 373 K.

It is expected that the principal error in the present model is in the calculation of ϕ_{2L}^{∞} . To improve upon our accuracy, fugacity coefficients of solutes for liquid, ϕ_{2L}^{∞} , have been evaluated from

$$\ln \phi_{2,L}^{\infty} = \ln K_{\rm D}(recom) + \ln \phi_{2,V}^{\infty}$$
⁽²³⁾

with $\ln K_{\rm D}(recom)$ calculated from Equation (13). The corrected values of ϕ_{21}^{∞} are given in the Excel file "Supplementary Materials".

3.3.2. Comparison of Henry's constants

Henry's constant, $k_{\rm H}$, is defined in Ref. [58] as

$$k_{\rm H} = \lim_{x_2 \to 0} (f_2 / x_2) \tag{24}$$

where f_2 and x_2 are the fugacity and mole fraction of a solute. The fugacity of a solute is given by $f_2 = P\phi_2 x_2$ [50]. Applying this definition to the vapor-liquid envelope of water, the relation between $k_{\rm H}$ and $K_{\rm D}$ is [26,59]:

$$k_{\rm H} = K_D \phi_{2,V}^{\infty} P_{1,s}^* \tag{25}$$

with $P_{1,s}^*$ the water saturation pressure. Using K_D values computed with Equation (13) in Equation (25), Henry's constants have been calculated for the solutes under consideration and compared with the recommendations of [58]. The results are shown in Fig. 8.

For Xe, N₂, and O₂ over the whole temperature range from 298.15 to 647.1 K (T_c) the agreement of recommended k_H values with those from Equation (25) is very good, within 0.08 ln units (<0.04 log₁₀ units); for Ne, Ar, and CH₄ the agreement is satisfactory – within 0.18 ln units (<0.08 log₁₀ units). However, for He, Kr, and H₂ the deviations increase significantly as *T* increases above 600 K. At 647.1 K (T_c) the differences are 1.3, 0.45, and 0.68 ln units, respectively (~0.6, 0.2 and 0.3 log₁₀ units). For CO, the disagreement begins at lower temperatures, growing from ~0.2 ln units (~0.09 log₁₀ units) at 500 K to more than 0.4 ln units (~0.18 log₁₀ units) for *T* > 550 K. The greatest deviations are generally at temperatures above those of the measurements.

The differences arise from using the present calculated values of $\phi_{2,V}^{\infty}$ and those estimated in Ref. [58] that employed the Peng-Robinson EOS. To assess which result should be accepted, values of $\phi_{2,V}^{\infty}$ have been calculated using B_{12} with Eq. (26) that should be sufficiently accurate up to approximately 1/2 the water critical density:

$$\ln \phi_{2,V}^{\infty} \approx \frac{2}{V_1^*} B_{12} - \ln \frac{PV_1^*}{RT}$$
(26)

The density of saturated water at $T \sim 633$ K is $\rho_1^* \approx 144$ kg m⁻³ or ~45% of the critical water density. Fig. 9 compares $\phi_{2,V}^{\infty}$ values from: 1) $k_{\rm H}$ and $K_{\rm D}$ data of [58]; 2) results of this work; 3) Equation (26) for He and CO. The Supplementary Material shows the results for all solutes where a comparison is possible.

Because the correct lower density formulation with B_{12} is incorporated in the present approach, the overall results of this work are very close to those from predictions of Equation (26). For He and CO, values of $\phi_{2,V}^{\infty}$ employed in Ref. [58] at temperatures above 450–500 K are systematically lower those evaluated from the truncated virial EoS. This suggests that the recommended values for $k_{\rm H}$ should be revised at least for He and CO.

Japas and Levelt Sengers [59] have derived a linear relationship for the asymptotic variation of $k_{\rm H}$ near the solvent's critical point,

$$RT \ln \frac{k_H}{f_1^*} = h_0 + A_{Kr} \frac{\left(\rho_{1,L}^* - \rho_{1,c}^*\right)}{\left(\rho_{1,c}^*\right)^2}$$
(27)

where f_1^* is the pure water fugacity, which can be calculated using an EoS for H₂O [63]. The present work suggests that the last term in Equation (27) should be appended by an expanded form, similar to that of Equation (13). This leads to a correlation that accurately reproduces k_H from 298.15 to 647.1 K ($\tau = 1 - T/T_c$):

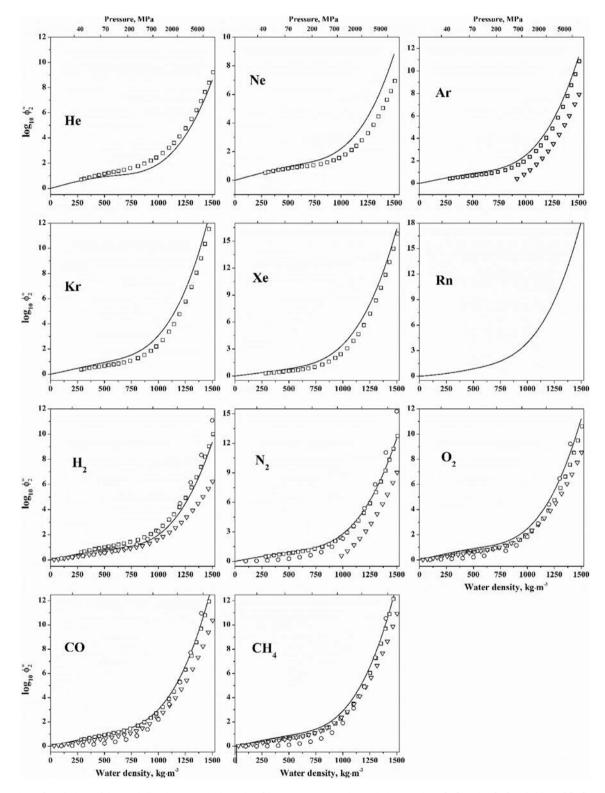


Fig. 5. Comparison of predictions of this work (lines) at 750 K with results of literature EoS, given by symbols: triangles – [11], circles ([12], coded by Ref. [14]), squares – [13].

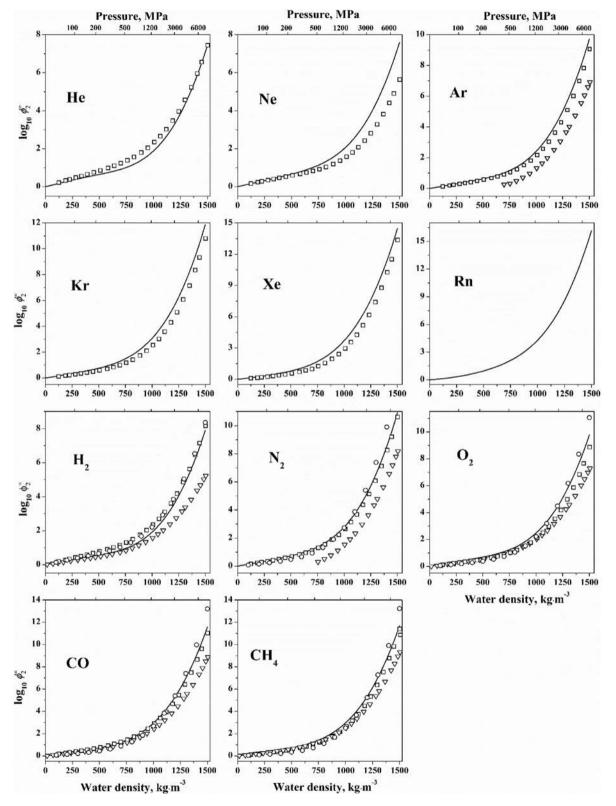


Fig. 6. Comparison of predictions of this work (lines) at 1500 K with results of literature EoS, given by symbols: triangles - [11], circles ([12], coded by Ref. [14]), squares - [13].

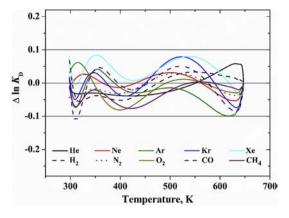


Fig. 7. The difference between recommended values of lnK_D [58] and those calculated with Equation (22).

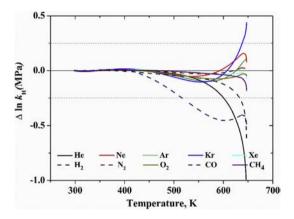


Fig. 8. Differences between recommended values of $lnk_{\rm H}$ [58] and those calculated with Equation (25).

$$RT \ln \frac{k_{H}}{f_{1}^{*}} = h_{0} + A_{Kr} \frac{\left(\rho_{1,L}^{*} - \rho_{1,c}^{*}\right)}{\left(\rho_{1,c}^{*}\right)^{2}} \left(1 + h_{1}\tau^{1.25} + h_{2}\tau^{1.5} + h_{3}\tau^{1.75} + h_{4}\tau^{2}\right).$$

$$(28)$$

where the parameters $h_0 - h_4$ are given in Table 6. This relation should not be used at temperatures outside of 298–647.1 K.

3.3.3. Calculation of ϕ_2^{∞} at high pressures (water densities) below T_c

Values of ϕ_2^{∞} along subcritical isotherms (T < 647.1 K) for compressed liquid water (for $P > P_{1,s}^*$, the water saturation pressure) can be obtained from

$$\ln \phi_{2}^{\infty} = \ln \phi_{2,L}^{\infty} + \rho_{1}^{*} \Big[a_{o} + \frac{a_{1}}{2} \rho_{1}^{*} + \frac{a_{2}}{3} (\rho_{1}^{*})^{2} + \frac{a_{3}}{4} (\rho_{1}^{*})^{3} + \frac{a_{4}}{5} (\rho_{1}^{*})^{4} \\ + \frac{a_{5}}{7} (\rho_{1}^{*})^{6} \Big] - \rho_{1,s}^{*} \Big[a_{o} + \frac{a_{1}}{2} \rho_{1,s}^{*} + \frac{a_{2}}{3} (\rho_{1,s}^{*})^{2} + \frac{a_{3}}{4} (\rho_{1,s}^{*})^{3} \\ + \frac{a_{4}}{5} (\rho_{1,s}^{*})^{4} + \frac{a_{5}}{7} (\rho_{1,s}^{*})^{6} \Big] - \ln \frac{P \rho_{1,s}^{*}}{P_{1,s}^{*} \rho_{1}^{*}},$$
(29)

where $\rho_{1,s}^*$ is the density of liquid water at $P_{1,s}^*$ and $\ln \phi_{2,L}^\infty$ is defined in Equation (23). Fig. 7 shows that the correction is small, always < 0.11 ln unit.

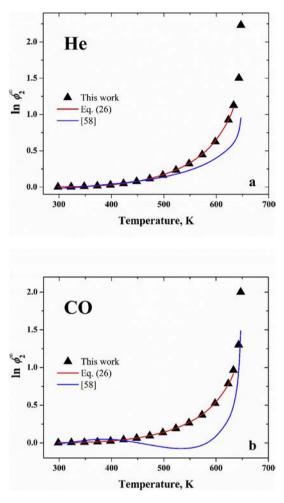


Fig. 9. The values of the fugacity coefficients evaluated in this work, calculated with Equation (26) and determined from $k_{\rm H}$ and $K_{\rm D}$ data of [58] for (a) He and (b) CO.

Values of parameters $h_0 - h_4$ of Equation (28) for calculating Henry's constants, $k_{\rm H}$, of solutes in water for *T* from 298.15 to 647.1 K.

Solute	h_0 , J mol ⁻¹	h_1	h ₂	h ₃	h_4
He	14101.4	-16.7925	64.5104	-79.1439	31.8977
Ne	14003.0	39.5335	-138.405	163.732	-65.1344
Ar	13082.5	49.6717	-181.137	225.384	-95.0142
Kr	12448.0	70.1943	-255.179	314.861	-131.292
Xe	10168.7	40.0254	-136.713	168.492	-73.2324
Rn	8611.8	28.5425	-128.408	198.412	-101.063
H ₂	13008.3	2.97582	-3.69394	0	0.871058
N ₂	13270.4	27.2763	-95.0488	117.070	-50.1020
02	13158.3	26.5351	-95.6743	120.939	-52.6848
CO	13017.7	72.6866	-266.528	331.484	-139.000
CH_4	12327.5	20.3832	-68.5418	84.8780	-37.5232

4. Summary

Table 6

Equations with parameters have been given for the thermodynamic properties of He, Ne, Ar, Kr, Xe, Rn, H₂, N₂, O₂, CO, and CH₄ at infinite dilution in water from 298 to 2000 K and water densities from 0 to 1500 kg m⁻³. Eq. (18) gives the correlation for A_{12}^{∞} . Eq. (21) gives the solute infinite-dilution fugacity coefficient, $\ln\phi_2^{\infty}$. This equation can be used directly at the critical isotherm and above, though small corrections are recommended at subcritical temperatures, in order to achieve the agreement with the vapor-liquid distribution coefficients, K_D of Eq. (13). In particular, we recommend using the small correction of Eq. (23) for the values of the $\phi_{2,L}^{\infty}$, the fugacity coefficient of an infinitely diluted solute in a liquid phase of water at saturation, calculated with Eq. (21). The values of Henry's constants, $k_{\rm H}$, consistent with $K_{\rm D}$ and fugacity coefficients for solutes in the vapor phase of water ($\phi_{2,V}^{\infty}$, calculated with Eq. (21)) are given by Eq. (28) over temperatures from 298.15 to 647.1 K. Calculated A_{12}^{∞} and ϕ_{2}^{∞} for all solutes at various *T* and *P* are tabulated in the Supplementary Material in an Excel file.

Examples are shown for aqueous methane. Fig. 10a shows A_{12}^{∞} for dissolved methane as a function of water density at various temperatures. Fig. 10b shows $\log_{10}\phi_2^{\infty}$ at the same conditions. The partial Gibbs energy may be defined as

$$G_2 = RT \ln \frac{P\phi_2^{\infty}}{P^{\circ}} \tag{30}$$

where $P^{\circ} = 0.1$ MPa for pressures given in MPa. Fig. 10c shows G_2 as a function of water density at various temperatures for dissolved

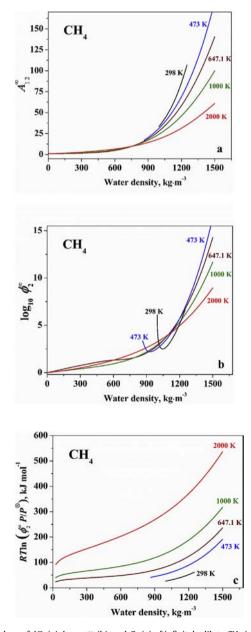


Fig. 10. Values of A_{12}^{∞} (a), $\log_{10}\phi_2^{\infty}$ (b), and G_2 (c) of infinitely dilute CH₄ in water over wide *T* and ρ_1^* ranges.

methane. Note that values of $\log_{10}\phi_2^{\infty}$ pass through minima at subcritical temperatures, though these are not seen in G_2 .

5. Conclusions

Equations have been developed for several thermodynamic properties of simple fluid solutes at infinite dilution in water from 298 to 2000 K and water densities from 0 to 1500 kg m⁻³. For this entire range of conditions, the method based on Fluctuation Solution Theory requires only very limited and well-known property values: the partial molar volume at infinite dilution, V_2^{∞} , of the solute at 298.15 K; the second cross virial coefficient of the solute with water, B_{12} , and the solute's Krichevskii parameter, A_{Kr} .

Fugacity coefficients, ϕ_2^{∞} , at supercritical temperatures agree reasonably with results of prior studies, suggesting that hightemperature thermodynamic properties of simple fluids at high dilution in water can now be considered known within restricted uncertainties. Small corrections were required to achieve agreement with the recommended [58] constants of distribution of solutes between the vapor and liquid phases of water, k_D . Comparisons of calculated Henry's constants with recommendations [58] suggest revision of results for some solutes when T > 550 K.

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Appendix A. Supplementary data

Supplementary data to this article can be found online at https://doi.org/10.1016/j.fluid.2019.06.012.

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